





# Polymer-Enhanced Fluid Effects on Mechanical Efficiency of Hydraulic Pumps

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## Viscosity Modifiers

- Viscosity modifiers (VMs) or viscosity index improvers (VIIs) are used in many hydraulic fluid formulations
- VM polymers thicken the fluid at high temperatures
- These additives help minimize the variation of viscosity during operation



Data replotted in Martini et al., *Tribol Lett* (2018) 66:58 from Ver Strate & Struglinski, In Schulz & Glass (eds.), *ACS*, Washington (1991)



# Shear Thinning

- VMs may experience high shear stress, causing temporary and permanent viscosity loss
- Our previous study showed that volumetric efficiency is more correlated to temporary viscosity loss [1]
- Project goal: understand how VMs and shear thinning of VM-containing fluids affect mechanical efficiency

[1] Michael et al. Tribol Trans (2018) 61:901
[2] Martini et al., Tribol Lett (2018) 66:58





### Axial Piston Pump: Critical Shear Rates

The major lubricating gaps in an axial piston pump exist between the interfaces indicated in red:



Modified from Shang & Ivantysynova, Energies 2018, 11(11), 3210

Significant viscous friction occurs at the following shear rates:

	Shear Rate Range [1/s]
Piston/cylinder	$8.85 \times 10^4 - 5.19 \times 10^5$
Slipper/swashplate	$8.42 \times 10^4 - 1.10 \times 10^6$
Cylinder block/valve plate	$1.00 \times 10^{6} - 8.58 \times 10^{6}$

Therefore, the approximate critical shear rate range in an axial piston pump is  $10^4 - 10^7 1/s$ 



#### Our Approach

#### **Molecular Simulations**



Molecular dynamics (MD) simulations performed in LAMMPS; Image rendered using OVITO

#### Viscosity Measurements



(Top) Cannon StressTech HR Oscillating Rheometer; (Bottom) PCS Ultra Shear Viscometer

#### **Pump Performance Tests**



Dynamometer showing Coriolis flow meter before the pump inlet which enables measurement of the fluid density

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## Test Fluids

- 3 hydraulic fluid formations were created to have the same viscosities but different concentrations of VMs
- All fluids were formulated with poly(isobutylene) (PIB) and/or poly(alphaolefin) (PAO)
- These formulations enable the effect of base oil viscosity reduction to be isolated

	HV46-1	HV46-2	HV46-3
Viscosity @ 40°C [cSt]	48.92	46.75	46.74
Viscosity @ 100°C [cSt]	8.89	8.08	7.86
Viscosity Index	164	146	138
Vis loss @ 40°C, D5621	0.84%	0.62%	0.36%
PAO 2 [wt.%]	61.5%		
PAO 4 [wt.%]		81.0%	
PAO 8 [wt.%]			100%
PIB [wt.%]	38.5%	19.0%	

\* All formulated with the same commercial anti-wear additive package



### **PIB and PAO Molecular Structures**

Polyisobutylene (1300 g/mol)



Dimer  $(C_{20})$  of 1-Decene

Trimer  $(C_{30})$  of 1-Decene







### **MD** Simulation Setup



38.4% PIB

HV46-1



20.4% PIB





# MD Simulation Validation

- To validate our MD simulations, we tested our viscosity prediction for HV46-1 at 100°C
- The average viscosity value and standard deviation were calculated from four independent simulations
- Reasonable predictions suggest that the simulations can be used to calculate viscosity trends where experimental data is not available

	Expected [cSt]	Simulation Prediction [cSt]	Error [cSt]
Viscosity	8.89	8.40 ± 3.31	0.49







## Shear Thinning in MD Simulations





### Shear Rate Range for Each Method

#### **UC Merced Rheometer**



Low Shear:  $1-1\times10^3$  1/s

Ultra Shear Viscometer



High Shear:  $1 \times 10^5 - 2 \times 10^6$  1/s

**Molecular Dynamics Simulations** 



Ultra High Shear:  $1 \times 10^9 - 1 \times 10^{11}$  1/s



#### Viscosity vs Shear Rate Results at 50°C



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### Dynamometer

- Pump performance testing was conducted for all fluids in a dynamometer per the ISO 4409 standard
- The dynamometer consists of:
  - 46cc variable displacement axial piston pump
  - Electronic swashplate control



Dynamometer showing Coriolis flow meter before the pump inlet which enables measurement of the fluid density



## Test Conditions

- Test points via Latin Hypercube method
- Pump testing parameters are shown in the table below:

Pump Testing Parameters		
Speed	600–2200 rpm	
Displacement	0-100%	
System Pressure	7–207 bar	
Nominal Fluid Temperature	50°C	





#### Dynamometer Results - Torque

Best subsets regression identified three model terms for pump input torque:

Term	Form
Theoretical (1)	$T_o = \frac{(V_i)p}{2\pi}$
Viscous (2)	$T_l = \mu \omega(V_i)$
Turbulent (3)	$T_t = \frac{\rho(V_i)^{\frac{5}{3}}}{4\pi}\omega^2$

(1) Wilson, 1950(2)Wilson,1950(3)Thoma, J., 1969



Model Torque, Nm



#### **Torque Residual Analysis**





#### Dynamometer Results – Idling Losses



- It appears that HV46-2 required the least idle torque and power input, followed by HV46-1 and HV46-3
- Hypothesis that reducing viscosity of the carrier base oil improves mechanical efficiency was not supported by the experimental results



#### Viscosity at the Critical Shear Rate Range



- Recall: the critical shear rate range in an axial piston pump was between 10<sup>4</sup> and 10<sup>7</sup> 1/s
- In this critical shear rate region,
  - HV46-1 has the highest viscosity and most shear thinning
  - HV46-2 has lower viscosity and moderate shear thinning
  - HV46-3 exhibits the least shear thinning



## Summary

- The effect of VMs was studied using three fluids with varying concentrations of PIB but the same 40 and 100°C viscosities
- Experiments and simulations captured the shear thinning behavior of these fluids across ten decades of shear rates
- Preliminary idle pump tests showed that the HV46-2 performed the best with lower torque and input power
- The range of shear rates at regions of high viscous friction and leakage flow was identified for an axial piston pump
- Future work will correlate shear thinning to hydraulic efficiency



# Thank You!



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